

## Active Refrigerators Powered by Inertia

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We present the operational principle for a refrigerator that uses inertial effects in active Brownian particles to locally reduce their (kinetic) temperature by 2 orders of magnitude below the environmental temperature. This principle exploits the peculiar but so-far unknown shape of the phase diagram of inertial active Brownian particles to initiate motility-induced phase separation in the targeted cooling regime only. Remarkably, active refrigerators operate without requiring isolating walls opening the route toward using them to systematically absorb and trap, e.g., toxic substances from the environment.

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**Introduction.**—Many processes in nature allow one to readily heat up an isolated system. Examples include the release of heat in chemical reactions occurring, e.g., when burning wood or gas, inelastic collisions occurring within resistors when exposed to electric currents, and mass-energy conversion processes in nuclear power plants and helium-burning stars. Following the second law of thermodynamics, none of these processes can be reverted, making us believe that it is impossible to cool down an isolated physical system. Accordingly, cooling down a target domain such as the inside of a refrigerator or atoms in a magneto-optical trap requires that the relevant domain is in contact with an external bath to which heat can be transferred via conduction, convection, radiation, or evaporation. Accordingly, developing sophisticated techniques to transfer heat from a target system to the environment has been a great challenge of 20th century physics [1–5].

For active systems [6–13], which consist of self-propelled particles and are intrinsically out of equilibrium, the second law does not apply to the active particles (but only to the overall system) [14]. Therefore, in the present Letter, we ask if it is possible to cool down a system of active Brownian particles (ABPs) [6,53] in a certain target

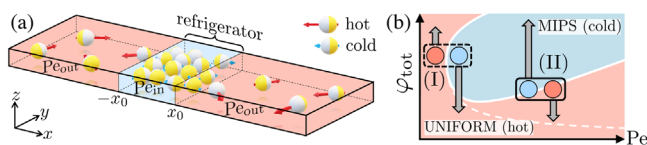


FIG. 1. Schematic of the active refrigerator (a), which exploits the peculiar shape of the phase diagram (b). The blue region represents phase coexistence (MIPS), and the white solid line represents the newly discovered transition line for inertial ABPs in comparison with the well-known transition line for overdamped ABPs (dashed line). Boxes and arrows refer to relevant parameter regimes discussed in the text.

region [refrigerator, Fig. 1(a)] in terms of their kinetic temperature [14] without requiring a mechanism to transfer energy to particles in the (spatially separated) environment.

To achieve this, we exploit the previous finding that ABPs can spontaneously phase separate into a dense and a dilute phase [motility-induced phase separation (MIPS)] [7,54–73]. While MIPS behaves similar to an equilibrium phase transition at large scales in the overdamped limit [59,63,73,74], in the presence of inertia, as relevant for, e.g., activated dusty plasmas [75,76] or vibrating granular particles [77–86], the coexisting phases feature different temperatures, which is, in contrast to clustering in granular gases caused by inelastic collisions [87–91], a consequence of self-propulsion and elastic collisions [92,93]. However, this finding alone is not sufficient to design an active refrigerator because it leads to a dense and cold phase, which occurs as randomly distributed clusters that move, merge, and coarsen and ultimately lead to a uniform temperature profile when averaging over many realizations or a long time [Fig. 2(a)].

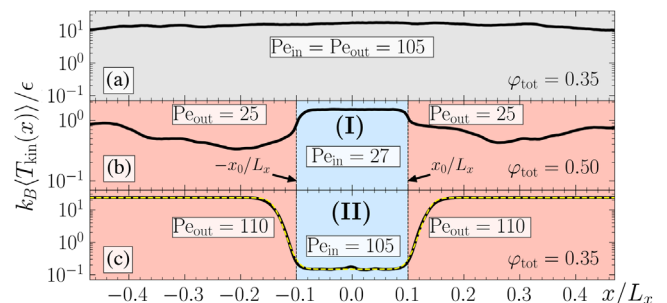


FIG. 2. Kinetic temperature profiles  $k_B T_{\text{kin}}(x) = m\langle|\vec{v}|^2\rangle_y/2$  in the steady state averaged over the  $y$  coordinate and 20 realizations with  $N = 16000$  particles for (a) uniform  $\text{Pe}$  and (b),(c) nonuniform  $\text{Pe}$  and parameters shown in the key. The yellow dashed line is a fit of  $f(x) = a\{2 - \tanh[b(x+c)] + \tanh[b(x-c)]\}/2 + d$ .

Thus, to create an active refrigerator, we need to meet the challenge of finding a mechanism allowing us to initiate MIPS in the targeted cooling domain only and to localize the dense phase in that region. To achieve this, one naive approach could be to implement a nonuniform motility [94,95] (e.g., through controlling the laser intensity in light-fueled swimmers [96–99]) such that particles in the targeted cooling domain show a (large) Péclet number [(Pe) relative importance of self-propulsion compared to diffusion] beyond the critical one for the MIPS phase transition, whereas particles in the environment feature a (small) subcritical Pe [Fig. 1(b), regime (I)]. However, this does not work because Pe and the density essentially behave inversely to each other [7,60] such that locally increasing Pe decreases the density in the same spatial region and does not result in a significant temperature difference [Fig. 2(b)]. Remarkably, however, the opposite strategy turns out to work in a carefully selected portion of the phase diagram [Fig. 1(b), regime (II)]: we find that reducing Pe in the targeted cooling domain by less than 5% as compared to the environment reduces the kinetic temperature of the ABPs by 2 orders of magnitude. This surprising finding exploits a remarkable difference between the phase diagram of inertial ABPs and the well-known phase diagram of overdamped ABPs: while MIPS occurs in overdamped ABPs when both Pe and the density are sufficiently large, in underdamped ABPs, it occurs at sufficiently large density and intermediate Pe. Thus, when choosing values of Pe within this intermediate regime in the targeted cooling domain and higher values in the environment, the density further increases in the former region, bringing the system deeper into the MIPS regime and further away from it outside. That is, inertia is required twice: first, to induce the two-temperature coexistence and second, to create the required shape of the phase diagram.

The resulting active refrigerator exemplifies a fundamentally new way to locally cool down a physical system. Like ordinary refrigerators, it can be used to cool down other objects. However, as opposed to ordinary cooling devices, active refrigerators use a self-organized cooling domain such that no isolating walls are required to separate the cooling domain from its environment. As a consequence, active refrigerators can, in principle, also be used as a device to absorb particles from the environment and to store them for a long time, as we shall see.

*Model.*—We consider inertial active Brownian particles [53,69,72,92,100,101] in two spatial dimensions. Each particle is represented by a (slightly soft) disk of diameter  $\sigma$ , mass  $m$ , and moment of inertia  $I = m\sigma^2/10$  and features an effective self-propulsion force  $\vec{F}_{\text{SP},i} = \gamma_t v_0 \hat{p}_i(t)$ , where  $v_0$ ,  $\hat{p}_i$  denote the (terminal) self-propulsion speed and the orientation  $\hat{p}_i(t) = (\cos \phi_i(t), \sin \phi_i(t))$  of the  $i$ th particle ( $i = 1, 2, \dots, N$ ), respectively. Position  $\vec{r}_i$  and orientation angle  $\phi_i$  evolve according to  $d\vec{r}_i/dt = \vec{v}_i$  and  $d\phi_i/dt = \omega_i$ ,

respectively, where the velocity  $\vec{v}_i$  and the angular velocity  $\omega_i$  in turn evolve as

$$m \frac{d\vec{v}_i}{dt} = -\gamma_t \vec{v}_i + \gamma_t v_0 \hat{p}_i - \sum_{\substack{j=1 \\ j \neq i}}^N \nabla_{\vec{r}_i} u(r_{ij}) + \sqrt{2k_B T_b \gamma_t} \vec{\xi}_i, \quad (1)$$

$$I \frac{d\omega_i}{dt} = -\gamma_r \omega_i + \sqrt{2k_B T_b \gamma_r} \eta_i. \quad (2)$$

Here,  $\gamma_t$  and  $\gamma_r$  are the translational and rotational drag coefficients, respectively, and  $T_b$  is the temperature of the bath, e.g., of the liquid or plasma medium surrounding the particles, which can differ from the kinetic temperature of the particles [102] and which we treat as constant in our simulations (see Supplemental Material [14]). The interaction potential  $u(r_{ij})$ ,  $r_{ij} = |\vec{r}_i - \vec{r}_j|$  is modeled by the Weeks-Chandler-Anderson potential [103] with strength  $\varepsilon$  and effective particle diameter  $\sigma$ . Finally,  $\vec{\xi}_i$  and  $\eta_i$  denote Gaussian white noise with zero mean and unit variance. We define  $\text{Pe} = v_0/\sqrt{2D_r D_t}$ , where  $D_t = k_B T_b/\gamma_t$  and  $D_r = k_B T_b/\gamma_r$  denote the translational and rotational diffusion coefficients, respectively. Note that ABP models like ours do not explicitly describe the self-propulsion mechanism, the underlying energy source, or how energy is dissipated into the bath [53,104]. We discuss possible experimental realizations below and develop a thermodynamically consistent picture in the paragraph “where does the energy flow?”.

In all simulations, we fix  $m/(\gamma_t \tau_p) = 5 \times 10^{-2}$ ,  $I/(\gamma_r \tau_p) = 5 \times 10^{-3}$ ,  $\varepsilon/(k_B T_b) = 10$ , and  $\sigma/\sqrt{D_r D_t} = 1$  with the persistence time  $\tau_p = 1/D_r$ . We choose  $\gamma_t = \gamma_r/\sigma^2$  and vary Pe and the total area fraction  $\varphi_{\text{tot}} = N\pi\sigma^2/(4A)$ , where  $A = L_x L_y$ ,  $L_y/L_x = 0.05$ , denotes the area of the simulation box. The Langevin equations are solved numerically with LAMMPS [105,106] for up to  $N = 10^5$  particles using periodic boundary conditions and a time step  $\Delta t/\tau_p = 10^{-5}$  (see Supplemental Material [14] for further details).

Our setup is illustrated in Fig. 1(a): the simulation area is divided into two regions, in which the particles have different Péclet numbers  $\text{Pe}(x_i) = v_0(x_i)/\sqrt{2D_r D_t}$ , i.e., the self-propulsion speed of each particle depends on its position according to

$$v_0(x_i) = \begin{cases} v_{0,\text{in}}, & -x_0 < x_i < x_0 \\ v_{0,\text{out}}, & \text{else} \end{cases}, \quad (3)$$

with  $x_0 \ll L_x$ . Note that our results are robust with respect to changes of  $x_0$ ,  $N$ ,  $m$ ,  $v_{0,\text{in}}$ , and  $v_{0,\text{out}}$  and, in particular, apply to values of  $m/(\gamma_t \tau_p)$  used in previous works [70,72,92,93,107,108] (Figs. S9–S12 in the Supplemental Material [14]). Initially, all particles are uniformly distributed in the whole simulation area.

*Active refrigerators.*—The goal is now to find  $Pe_{in}$  and  $Pe_{out}$  such that (i) MIPS occurs in the targeted cooling domain only and (ii) the resulting dense phase stays in that region. Notice first that, when choosing  $Pe_{in} = Pe_{out}$ , in each individual realization, we find different kinetic temperatures in coexisting phases, but the ensemble-averaged (or time-averaged) kinetic temperature profile is uniform [Fig. 2(a)]. If we choose  $\varphi_{tot} = 0.5$  and  $Pe_{in} > Pe_{out}$  [regime (I) in Fig. 1(b)] to trigger MIPS in the target domain only, however, we obtain only a weak temperature difference (which even goes in the wrong direction), because the particle density compensates the difference in  $Pe$  (because the residential time of a particle in a small volume element scales inversely to its speed) as indicated by the gray arrows in Fig. 1(b) (note that the arrow length depends on the density of both phases and thus is not obvious). More generally, when choosing other combinations  $Pe_{in} > Pe_{out}$  and density in the left part of the phase diagram [Fig. 1(b), regime (I)], we do not observe any relevant cooling in the target domain. Remarkably, however, if we choose a comparatively low area fraction of  $\varphi_{tot} = 0.35$  and  $Pe_{in} = 105 < Pe_{out} = 110$  [regime (II) in Fig. 1(b)], we observe that the system undergoes MIPS exclusively in the target domain and the dense phase remains in that region (Movie M1 in the Supplemental Material [14]). This results in a striking cooling effect by more than 2 orders of magnitude in the cooling domain from  $k_B \langle T_{kin}^{(out)} \rangle / \varepsilon \approx 23.4$  to  $k_B \langle T_{kin}^{(in)} \rangle / \varepsilon \approx 0.147$  [Fig. 2(c)], which is further enhanced when choosing larger  $Pe$  differences and complemented by a significantly lower entropy production rate in the cooling domain and an inward flow of kinetic energy (Figs. S3–S5 in the Supplemental Material [14]).

*Phase diagram.*—To understand the possible parameter choices for constructing active refrigerators in detail, we now discuss the phase diagram of inertial ABPs in the  $Pe$ - $\varphi_{tot}$  plane, which has remained unknown to date. The key control parameters of the system are  $\varepsilon$ ,  $Pe$ , and  $\varphi_{tot}$  for fixed  $m$  and  $I$ . We additionally fix  $\varepsilon$  and vary  $Pe$  and  $\varphi_{tot}$ . To determine the transition line between the uniform state and the MIPS regime (Fig. 3), we investigate the distribution of the local area fraction  $\varphi_{loc}$  [67,72,109], which is unimodal in the uniform regime and bimodal in the coexistence regime (Fig. S1 in the Supplemental Material [14]). Interestingly, the transition line does not follow the well-known relation  $Pe \propto 1/\varphi_{tot}$ , which was found in the overdamped regime [54,56]. In striking contrast, we find that  $Pe \propto \varphi_{tot}$  in the large  $Pe$  regime (green part of the transition line in Fig. 3). This relation serves as a crucial ingredient to construct an active refrigerator. Intuitively, it can be understood to occur as a direct consequence of inertial effects: the particles bounce back when they collide with each other and the rebound is much stronger for large  $Pe$  than for moderate  $Pe$ . Therefore, to slow down locally, more

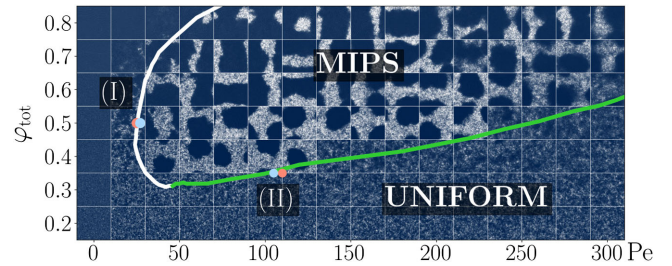


FIG. 3. Phase diagram of  $N = 20\,000$  inertial ABPs (background images are steady-state snapshots). The solid line shows the transition line (see Supplemental Material [14] for details). In the vicinity of its green part, parameters can be chosen to construct active refrigerators.

collisions are necessary and a larger area fraction is required at larger  $Pe$  to initiate MIPS.

*Design rule.*—Based on the transition line, we can formulate the following strategy to realize the active refrigerator: first, we want to initiate MIPS in the target domain. This can be achieved by choosing  $(Pe_{in}, \varphi_{in})$  inside the MIPS region of the phase diagram for the target domain. Second, we do not want the system to undergo MIPS outside the target domain. Hence, we choose  $(Pe_{out}, \varphi_{out})$  outside the coexistence region. Third, we want the particle flux that emerges as a consequence of choosing two different Péclet numbers to bring the system deeper into the coexistence regime within the target domain but further away from it outside. Clearly, based on the obtained detailed knowledge of the phase transition line, the first two criteria can be easily met by fixing a suitable area fraction  $\varphi_{in} = \varphi_{out} = \varphi_{tot}$  and choosing two Péclet numbers on both sides of the transition line. However, the third criterion can only be met by choosing parameter combinations in the vicinity of the green marked part of the transition line [regime (II)]. To see this, we will next discuss the particle flux that emerges when choosing two different Péclet numbers.

*Supportive and counteracting feedback.*—Let us first recall that the mean speed of an ABP decreases with increasing  $\varphi_{tot}$  and increases with increasing  $Pe$  (Fig. S2 in the Supplemental Material [14]). Consequently, when we have two regions with different Péclet numbers, a lower density will emerge in the high- $Pe$  region and a larger one in the low- $Pe$  region. Therefore, the gray arrows in Fig. 1(b) always point to lower  $\varphi_{tot}$  at the high- $Pe$  point and vice versa.

In regime (I) and, more generally, in the vicinity of the white part of the transition line in Fig. 3, we need to choose  $Pe_{in} > Pe_{critical} > Pe_{out}$  to initiate MIPS in the target domain only. Consequently, the density initially decreases in that region [Fig. 4(a)]. Interestingly, the area fraction in the target domain typically decreases to values below the transition line even for a relatively small  $Pe$  difference, which fully prevents MIPS in the target domain.

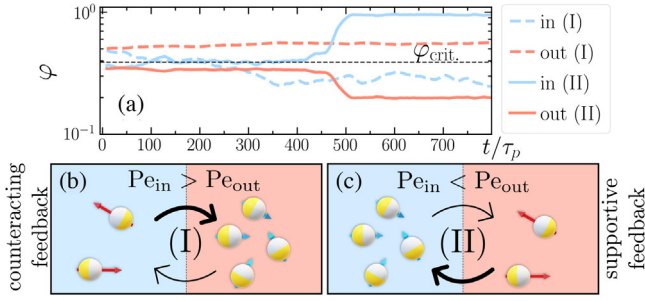


FIG. 4. (a) Area fraction in inner and outer regions over time for regime (I) and (II) (parameters as in Fig. 2). The dashed horizontal line shows the critical area fraction  $\phi_{crit} \approx 0.39$  for  $Pe = 27$ . A (b) counteracting [(c) supportive] feedback loop decreases [increases] the particle density in the target region.

This surprisingly strong decrease can be viewed as the result of a positive feedback loop [Fig. 4(b)]: the decrease of the particle density in the target domain increases the mean speed of the particles in that region, which further decreases the particle density in the target domain. Thus, no cooling occurs within that region (but rather the opposite, see Fig. 2). In stark contrast, following the peculiar shape of the phase transition line at large  $Pe$  (Fig. 3), the initial particle flux points in the right direction and gives rise to the enormous cooling effect for only tiny differences in  $Pe$ . More specifically, when choosing  $Pe_{in} < Pe_{critical} < Pe_{out}$  [as in regime (II)], the particles are initially faster in the environment, which enhances the density inside the target domain where MIPS occurs and further slows down the particles, which further supports the particle flux from the environment [Fig. 4(c)].

*Where does the energy flow?*—The finding of a persistent temperature gradient for the active particles is measurable with a suitable thermometer (Supplemental Material [14]) and does, of course, not contradict thermodynamics: heat always flows from hot to cold within the bath (solvent or gas) that surrounds the active particles. This heat flow persists in steady state and is maintained by the (external) energy source driving the system: let us imagine light-powered Janus colloids in a liquid [6] or a complex plasma [75,76], where inertia is important. Clearly, in steady state, when neglecting temperature changes of the particle material, essentially all the energy that is absorbed by the active particles from the external light source is ultimately transferred to the bath. That is, for a uniform  $Pe$  (defocused laser), the particles act as identical heat sources for the bath. When realizing active refrigerators with a slightly nonuniform  $Pe$  ( $Pe_{out} \gtrsim Pe_{in}$ ), we obtain a significantly enhanced particle density within the refrigerator region and, hence, a comparatively hot solvent. Thus,  $T_b$  is large in regions where  $T_{kin}$  is low, leading to a persistent bath energy flow from hot to cold (see Supplemental Material [14] for a minimal model of  $T_b$ ). Note that changes in  $T_b$  are small compared to changes in

$T_{kin}$  since the bath has many degrees of freedom. Hence, we keep  $T_b$  constant (as typical for ABP models [6]). (This argument is, of course, not restricted to light-powered swimmers but essentially applies also to, e.g., chemically powered swimmers when considering the fuel as an external energy source.)

The direction of the bath energy flow can also be spatially reverted: for  $Pe_{out} \gg Pe_{in}$ , the bath heats up stronger outside the refrigerator region because the light absorption grows faster than the particle density inside, which cannot exceed close packing [14]. Then, heat flows into the refrigerator region within the bath but still from hot to cold.

*Absorbing, trapping, and cooling tracers with active refrigerators.*—One unique feature of the proposed active refrigerators is that they cool down colloidal particles in a certain region in space without requiring any isolating walls separating the cooling domain from the environment. Since the kinetic temperature differences are much larger than the temperature differences in the underlying bath, active refrigerators can also be used to absorb sufficiently large substances from the environment and to trap them for a long time (Fig. 5). To demonstrate this, we have performed simulations of inertial ABPs [parameters as in Fig. 2(c)] and additional passive tracer particles, which may represent, e.g., certain toxic substances and are randomly distributed outside the cooling domain. Remarkably, the active refrigerator systematically absorbs tracers from the environment and cools them by 2 orders of magnitude below the kinetic temperature of tracers outside the refrigerator domain [Fig. 5(a)]. Note that it can take a long time before a tracer enters the cooling domain, but once it is deep inside this region it stays there for a very long time, as indicated by the exemplary trajectories in Fig. 5(b) and Movie M2 in the Supplemental Material [14].

*Possible experimental realizations.*—Active refrigerators can be realized with self-propelled particles featuring significant inertia and elastic collisions such as activated microparticles in a plasma [75,76], mesoscopic propellers such as vibrated granular particles [77–85], drones [86,110,111], and minirobots [112], and dense animal

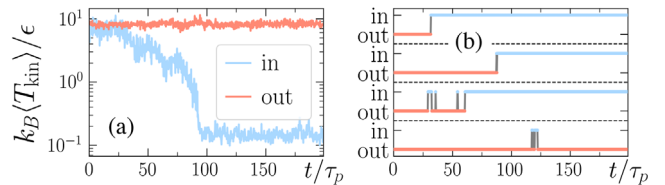


FIG. 5. Absorbing, trapping, and cooling tracers with active refrigerators. (a) Kinetic temperature of passive tracers inside and outside the cooling domain. (b) Position (inside or outside the cooling domain) of four exemplary passive tracers over time [parameters as in Fig. 2(c), but with  $Pe_{in} = Pe_{out} = 0$  for passive tracers and  $N_{passive}/N = 0.02$ ].

collections [113] such as swimming whirligig beetles, as recently demonstrated in Ref. [114].

*Conclusions.*—We have proposed a mechanism for an active refrigerator, which requires inertia not only to create a temperature difference across coexisting phases but also to induce the peculiar shape of the MIPS phase transition line, which we exploit to localize the cooling domain in a predefined region of space. As their key feature, active refrigerators create a self-organized cooling domain, in which active particles feature a much lower kinetic temperature compared to their environment. As they do not require any isolating walls to separate the cooling domain from its environment, active refrigerators prove a route toward possible future applications, e.g., to trap and absorb large (toxic) molecules or viruses. Overall, we found that the active-particle subsystem alone does not behave as one might expect from the laws of thermodynamics, but makes the bath pay the thermodynamic bill for a self-organized cooling domain that does not decay. This could be further explored within microscopic theories [115,116].

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